TTK4150 Nonlinear Control Systems Exercise 6 Part 2

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Exercise 1

In the following we are going to develop a control law for a spacecraft based on passivity. The model of the spacecraft is described with two state vectors. The orientation dynamics is given by

$$\phi = R\left(\phi\right)\omega$$

and the Euler equations for a rotating rigid spacecraft are given by

$$J_{1}\dot{\omega}_{1} = (J_{2} - J_{3})\omega_{2}\omega_{3} + \tau_{1}$$

$$J_{2}\dot{\omega}_{2} = (J_{3} - J_{1})\omega_{3}\omega_{1} + \tau_{2}$$

$$J_{3}\dot{\omega}_{3} = (J_{1} - J_{2})\omega_{1}\omega_{2} + \tau_{3}$$

where $\phi = [\phi_1 \ \phi_2 \ \phi_3]^T$ is the orientation vector, $\omega = [\omega_1 \ \omega_2 \ \omega_3]^T$ is a vector of angular velocity along the principal axes, $\tau = [\tau_1 \ \tau_2 \ \tau_3]^T$ is a vector of torque inputs applied about the principal axes and J_i are the principal moments of inertia. Further, we have that $R(\phi) = R^T(\phi)$ and we assume that $R(\phi)$ is non singular in our domain of interest $(R(\phi)$ is non singular on D_{ϕ} but not on \mathbb{R}^3).

- 1. Before we start with the passivity analysis and control design, the model properties are investigated and located.
 - (a) Verify that the system may be rewritten in a compact form as

$$\dot{\phi} = R(\phi) \omega$$

 $M\dot{\omega} = C(\omega) \omega + \tau$

where M is positive definite and symmetric and $C(\omega)$ skew symmetric.

- (b) We are solving the feedback stabilization problem for the spacecraft. Our stabilization problem is defined as stabilizing the system with a desired orientation and zero angular velocity. In order to apply our theoretical tools we need to rewrite the system such that origin is the point of interest. Let $e_1 = 0$ and $e_2 = 0$ describe the point of interest of ϕ and ω respectively, and rewrite the system in these variables.
- 2. Passivity based control consists mainly of two steps; locating a suitable input-output pair based on passivity and force some stronger passivity properties to the input-output pair, if not already present. We will conduct our passivity analysis using the storage function

$$V(e) = \frac{1}{2}e_2^T M e_2 + \frac{1}{2}e_1^T K_p e_1$$

where $K_p = K_p^T > 0$. In our case the control input is given by τ , and we only need to find a suitable measurement (output).

- (a) What physical interpretation can be made of the storage function.
- (b) Find a suitable output based on passivity analysis. Justify your answer.
- (c) Does the system have any passivity properties with respect to your choice of output and τ .
- 3. The next step, after having chosen a suitable output, is to force some passivity property on the system using the control input.
 - (a) Find a control input $\tau(\phi, \omega, v)$ such that the system is passive (lossless) from v to your choice of output.
 - (b) Comment on stability properties achieved with this control input.
 - (c) Find a control input $\tau(\phi, \omega, v)$ such that the system is output strictly passive from v to your choice of output.
 - (d) What are the differences of the control input turning the system output strictly passive with respect to the control input turning the system passive? Give a physical interpretation.
 - (e) Comment on stability properties achieved with this control input.

- 4. Suppose that we desire a more complex control law for the overall system. We desire to add control without making any calculations.
 - (a) Which of the previous control laws would you base your extension on? Justify the choice.
 - (b) The initial control law $\tau(\phi, \omega, 0)$ is troubled with a steady state deviation in the rotational velocity. Propose a control law that is likely to solve this problem. Is it possible to use the same approach to cope with a steady state deviation of the orientation.
 - (c) What can be said of the robustness with respect to uncertainty in measurements and actuators of the proposed system.

Exercise 2 (Exercise 14.30 a) in Khalil)

Exercise 3 (Exercise 14.31 in Khalil)

Exercise 4 (Exercise 14.34 in Khalil)